43960 measured reflections

 $R_{\rm int} = 0.049$

7095 independent reflections

5413 reflections with $I > 2\sigma(I)$

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Poly[[bis[μ_2 -1,3-bis(phenylsulfanyl)propane- $\kappa^2 S:S'$]silver(I)] hexafluoridoantimonate diethyl ether hemisolvate]

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Key indicators: single-crystal X-ray study; T = 220 K; mean σ (C–C) = 0.008 Å; some non-H atoms missing; disorder in main residue; R factor = 0.044; wR factor = 0.114; data-to-parameter ratio = 18.9.

The title compound, {[Ag($C_{15}H_{16}S_{2}$)₂]SbF₆·0.5C₄H₁₀O}_n, was obtained from the self-assembly of AgSbF₆ and 1,3-bis-(phenylsulfanyl)propane. Each Ag^I ion is coordinated by four S atoms from different ligands, forming a distorted tethrahe-dral geometry. Each ligand links adjacent Ag^I ions, forming an extended two-dimensional grid-like framework. SbF₆⁻ ions, which are incorporated into the cavities of the network, complete and stabilize the structure. One of the phenyl rings is disordered over two sites, the ratio of occupancies being 0.508 (4):0.492 (4).

Related literature

For related literature, see: Awaleh *et al.* (2006*a*,*b*, 2007); Black *et al.* (1995); Blake *et al.* (1999); Bu *et al.* (2002); Carlucci *et al.* (2002); Hartley *et al.* (1979); Hou *et al.* (2005); Millward & Yaghi (2005); Noro *et al.* (2002); Sluis & Spek (1990); Spek (2003); Withersby *et al.* (1997, 1999); Wong-Foy, Matzger & Yaghi (2006).



Experimental

Crystal data

N

h

$Ag(C_1 H_1 S_2) = BbE_{c} = 0.5C_4 H_{10}O$	$V = 3614.10(9) \text{ Å}^3$
$I_r = 901.52$	Z = 4
Aonoclinic, $P2_1/c$	Cu $K\alpha$ radiation
= 13.5794 (2) Å	$\mu = 12.87 \text{ mm}^{-1}$
= 13.0497 (2) Å	T = 220 (2) K
= 20.5848 (3) Å	$0.27 \times 0.14 \times 0.11 \text{ mm}$
$B = 97.791 \ (1)^{\circ}$	

Data collection

Bruker SMART 2K diffractometer Absorption correction: multi-scan (*SADABS*; Sheldrick, 1996) $T_{min} = 0.162, T_{max} = 0.239$

Refinement

$R[F^2 > 2\sigma(F^2)] = 0.044$	375 parameters
$vR(F^2) = 0.114$	H-atom parameters constrained
S = 0.95	$\Delta \rho_{\rm max} = 1.07 \ {\rm e} \ {\rm \AA}^{-3}$
7095 reflections	$\Delta \rho_{\rm min} = -0.92 \text{ e} \text{ Å}^{-3}$

Table 1

Selected geometric parameters (Å, °).

Ag1-S2	2.5293 (12)	Ag1-S4	2.5639 (12)
Ag1-S3	2.5621 (12)	Ag1-S1	2.6170 (12)
S2-Ag1-S3	118.58 (4)	S2-Ag1-S1	106.61 (4)
S2-Ag1-S4	114.28 (4)	S3-Ag1-S1	103.08 (4)
\$3-Ag1-\$4	109.98 (4)	S4-Ag1-S1	102.26 (4)

Data collection: *SMART* (Bruker, 1999); cell refinement: *SAINT* (Bruker, 1999); data reduction: *SAINT*; program(s) used to solve structure: *SHELXS97* (Sheldrick, 1997); program(s) used to refine structure: *SHELXL97* (Sheldrick, 1997); molecular graphics: *SHELXTL* (Bruker, 1997); software used to prepare material for publication: *UdMX* (Maris, 2004).

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Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: LH2544).

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Poly[[bis[μ_2 -1,3-bis(phenylsulfanyl)propane- $\kappa^2 S:S'$]silver(I)] hexafluoridoantimonate diethyl ether hemisolvate\]

M. O. Awaleh, A. Badia and F. Brisse

Comment

The self-assembly of metal-organic coordination polymers has attracted a great attention because of their potential as functional materials (Millward & Yaghi, 2005; Wong-Foy et al., 2006). When flexible ligands are involved in supramolecular architectures, the prediction of the topology of the coordination polymer is more difficult because there are several factors affecting the framework formation, such as the type of solvent, the counter-anion, and the metal-to-ligand ratio among others (Withersby et al., 1999, 1997; Noro et al., 2002; Black et al., 1995; Blake et al., 1999; Bu et al., 2002; Carlucci et al., 2002). Neverthless, in order to gain more information about those subtle factors, not yet well understood, we have studied the effect of one parameter at a time on the topology of the networks (Awaleh et al., 2006a,b; 2007). In our continuous effort to study the structure of the metal-organic supramolecular architecture, we report herein a silver(I) coordination polymer forming a lamellar network by using a flexible dithioether, viz. 1,3-bis(phenylsulfanyl)propane (L^{3-Ph}), as building block, namely Poly[Silver(I)-di-µ-1,3-bis(phenylsulfanyl)propane]hexafluoroantimonate acetone solvate (I). In the title complex (I), each Ag^{I} center is linked in a tetrahedral manner to a sulfur atom of four different L^{3-Ph} ligands (Fig. 1). The other sulfur atom of each ligand is bound to a neighbouring Ag^I ion thus forming a two-dimensional cationic coordination polymer where the repeat unit is a rectangular 24-membered macrometallocycle $Ag_4(L^{3-Ph})_4$ (Fig. 2). The phenyl groups of the L^{3-Ph} ligands are located on the same side of the Ag₄ plane. The dihedral angle between the phenyl groups is $71.6(20^{\circ})$. The PF₆⁻ ions are incorporated in the cavities of the repeating unit to balance the charge of the cationic coordination polymer (Fig. 3). Neighbouring rectangular rings are fused in a parquet-like pattern to form an infinite lamellar (4,4) coordination network (Fig. 3).

Experimental

The ligand 1,3-bis(phenylsulfanyl)propane, L^{3-Ph} , was synthesized following a publish report (Hartley *et al.*, 1979). For the synthesis of the title compound (I), a solution of AgSbF₆ (164 mg, 0.48 mmol) in acetone (5 ml) was added a solution of L^{3-Ph} (0.22 ml, 0.95 mmol) in diethyl ether (5 ml). The mixture was kept under reflux at 323 K for 2 h. The filtrate was recrystallized by diffusion of petroleum ether into the solution at room temperature. A few days later, single crystals suitable for X-ray analysis were deposited. Yield 74% based on AgSbF₆. Anal. Found: C, 42.46; H, 3.84. Calculated for C₃₂H₃₇S₄O_{0.5}AgSbF₆: C, 42.63; H, 4.14. ¹H NMR (DMSO-d₆, 400 MHz): d 1.84 (qt, 2H, -S-(CH₂)-(CH₂)-), 3.07 (t, 4H, -S-(CH₂)-), 7.28–7.59 (m, 10H, C₆H₅-). ¹⁹F NMR (DMSO-d₆, 376.31 MHz): d -137.49 - -102.91 (m, F—Sb).

Refinement

All non-H atoms were refined by full-matrix least-squares with anisotropic displacement parameters. H atoms were generated geometrically (C—H distances of 0.93 A for aromatic H, 0.97 A for the other) and were included in the refinement in

the riding model approximation; their temperature factors were set to 1.2 times those of the equivalent isotropic temperature factors of the parent site. An electron density map showed two regions centered at (1/2, 0, 0) and (1/2, 1/2, 1/2), containing peaks due to severely disordered solvent. No consistent models for diethyl ether molecules, which was the only solvent present, could be assembled from these peaks. This part of the structure was modeled by using the SQUEEZE procedure of *PLATON* (Spek, 2003), which indicated the presence of two cavities of 205 Å³, each occupied by 40 electrons, which is consistent with the presence of one CH₃CH₂OCH₂CH₃ molecule per cavity (half of diethyl ether molecule per asymmetric unit). The contribution of the disordered solvent was calculated with BYPASS (van der Sluis & Spek, 1990) and a new data set without the solvent contribution was generated. The final model consisting of the ordered part only was refined. One phenyl group of one 1,3-bis(phenylsulfanul)propane ligand was found to be disordered. This group was split over two sites with occupancies of 58 and 42%.

Figures



Fig. 1. The aysymmetric unit of the title compound. Ellipsoid are drawn at the 30% probability level. The disordered components are labeled with suffixes A and B.



Fig. 2. View of the 24-membered $Ag_4(L^{3-Ph})_4$ macrometallocyclic repeat unit of the title compound.



Fig. 3. View of the two-dimensional molecular-rectangle network of the title compound.

Poly[[bis[μ_2 -1,3-bis(phenylsulfanyl)propane- $\kappa^2 S:S'$]silver(I)] hexafluoridoantimonate diethyl ether hemisolvate]

Crystal data $[Ag(C_{15}H_{16}S_{2})_{2}]SbF_{6} \cdot 0.5C_{4}H_{10}O$ $M_{r} = 901.52$ Monoclinic, $P2_{1}/c$ Hall symbol: -P 2ybc a = 13.5794 (2) Å

 $F_{000} = 1712$ $D_x = 1.657 \text{ Mg m}^{-3}$ Cu Ka radiation $\lambda = 1.54178 \text{ Å}$ Cell parameters from 7995 reflections $\theta = 3.3-72.8^{\circ}$

b = 13.0497 (2) Å	$\mu = 12.87 \text{ mm}^{-1}$
c = 20.5848 (3) Å	T = 220 (2) K
$\beta = 97.7910 \ (10)^{\circ}$	Block, colorless
$V = 3614.10 (9) \text{ Å}^3$	$0.27\times0.14\times0.11~mm$

Z = 4

Data collection

Bruker SMART 2K diffractometer	7095 independent reflections
Radiation source: X-ray Sealed Tube	5413 reflections with $I > 2\sigma(I)$
Monochromator: graphite	$R_{\rm int} = 0.049$
Detector resolution: 5.5 pixels mm ⁻¹	$\theta_{\rm max} = 72.9^{\circ}$
T = 220(2) K	$\theta_{\min} = 3.3^{\circ}$
ω scans	$h = -16 \rightarrow 16$
Absorption correction: multi-scan (SADABS; Sheldrick, 1996)	$k = -13 \rightarrow 15$
$T_{\min} = 0.162, \ T_{\max} = 0.239$	$l = -25 \rightarrow 25$
43960 measured reflections	

Refinement

Refinement on F^2	Secondary atom site location: difference Fourier map
Least-squares matrix: full	Hydrogen site location: inferred from neighbouring sites
$R[F^2 > 2\sigma(F^2)] = 0.044$	H-atom parameters constrained
$wR(F^2) = 0.114$	$w = 1/[\sigma^2(F_0^2) + (0.0718P)^2]$ where $P = (F_0^2 + 2F_c^2)/3$
<i>S</i> = 0.95	$(\Delta/\sigma)_{\text{max}} = 0.001$
7095 reflections	$\Delta \rho_{max} = 1.07 \text{ e } \text{\AA}^{-3}$
375 parameters	$\Delta \rho_{min} = -0.92 \text{ e } \text{\AA}^{-3}$
Determine the state of the stat	

Primary atom site location: structure-invariant direct methods Extinction correction: none

Special details

Experimental. X-ray crystallographic data for I were collected from a single-crystal sample, which was mounted on a loop fiber. Data were collected using a Bruker Platform diffractometer, equipped with a Bruker *SMART* 2 K Charged-Coupled Device (CCD) Area Detector using the program *SMART* and normal focus sealed tube source graphite monochromated Cu—K α radiation. The crystal-to-detector distance was 4.908 cm, and the data collection was carried out in 512 *x* 512 pixel mode, utilizing 4 *x* 4 pixel binning. The initial unit-cell parameters were determined by a least-squares fit of the angular setting of strong reflections, collected by a 9.0 degree scan in 30 frames over four different parts of the reciprocal space (120 frames total). One complete sphere of data was collected, to better than 0.8Å resolution. Upon completion of the data collection, the first 101 frames were recollected in order to improve the decay correction analysis.

Geometry. All e.s.d.'s (except the e.s.d. in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell e.s.d.'s are taken into account individually in the estimation of e.s.d.'s in distances, angles and torsion angles; correlations

between e.s.d.'s in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell e.s.d.'s is used for estimating e.s.d.'s involving l.s. planes.

Refinement. Refinement of F^2 against ALL reflections. The weighted *R*-factor *wR* and goodness of fit *S* are based on F^2 , conventional *R*-factors *R* are based on *F*, with *F* set to zero for negative F^2 . The threshold expression of $F^2 > \sigma(F^2)$ is used only for calculating *R*-factors(gt) *etc*. and is not relevant to the choice of reflections for refinement. *R*-factors based on F^2 are statistically about twice as large as those based on *F*, and *R*-factors based on ALL data will be even larger.

	x	у	Ζ	$U_{\rm iso}*/U_{\rm eq}$	Occ. (<1)
Ag1	0.25367 (2)	0.61376 (3)	0.245888 (17)	0.02260 (10)	
Sb1	0.22596 (3)	0.08152 (3)	0.166843 (17)	0.03613 (11)	
S 1	0.21540 (8)	0.77327 (9)	0.31534 (6)	0.0215 (2)	
S2	0.34586 (8)	0.48708 (9)	0.32496 (6)	0.0252 (3)	
S 3	0.08207 (8)	0.56386 (9)	0.18682 (6)	0.0227 (2)	
S4	0.35897 (8)	0.69189 (9)	0.16407 (6)	0.0247 (3)	
F1	0.1398 (3)	0.1928 (3)	0.1844 (2)	0.0678 (12)	
F2	0.3345 (3)	0.1719 (4)	0.1855 (2)	0.0820 (15)	
F3	0.3054 (3)	-0.0257 (4)	0.1523 (2)	0.0916 (17)	
F4	0.1130 (3)	-0.0011 (3)	0.15182 (17)	0.0519 (9)	
F5	0.2087 (3)	0.1186 (4)	0.07860 (18)	0.0787 (15)	
F6	0.2400 (3)	0.0490 (3)	0.25589 (16)	0.0488 (9)	
C11	0.1783 (3)	0.7220 (4)	0.3894 (2)	0.0218 (10)	
C12	0.0832 (4)	0.6887 (4)	0.3940 (2)	0.0291 (11)	
H12	0.0343	0.6927	0.3578	0.035*	
C13	0.0607 (4)	0.6496 (4)	0.4522 (3)	0.0368 (13)	
H13	-0.0039	0.6285	0.4555	0.044*	
C14	0.1326 (5)	0.6415 (4)	0.5055 (3)	0.0444 (15)	
H14	0.1172	0.6140	0.5445	0.053*	
C15	0.2281 (5)	0.6742 (4)	0.5010 (3)	0.0394 (14)	
H15	0.2769	0.6687	0.5372	0.047*	
C16	0.2515 (4)	0.7153 (4)	0.4431 (3)	0.0330 (12)	
H16	0.3157	0.7382	0.4402	0.040*	
C17	0.1015 (4)	0.8260 (4)	0.2720 (2)	0.0251 (10)	
H17A	0.1135	0.8492	0.2290	0.030*	
H17B	0.0513	0.7726	0.2659	0.030*	
C18	0.0624 (3)	0.9153 (4)	0.3087 (2)	0.0231 (10)	
H18A	0.1110	0.9701	0.3135	0.028*	
H18B	0.0518	0.8931	0.3523	0.028*	
C21	0.2527 (3)	0.4021 (4)	0.3470 (2)	0.0244 (10)	
C22	0.2337 (4)	0.3056 (4)	0.3204 (3)	0.0284 (11)	
H22	0.2714	0.2799	0.2896	0.034*	
C23	0.1570 (4)	0.2476 (4)	0.3405 (3)	0.0317 (12)	
H23	0.1438	0.1824	0.3233	0.038*	
C24	0.1006 (4)	0.2860 (4)	0.3857 (3)	0.0339 (12)	
H24	0.0488	0.2472	0.3983	0.041*	
C25	0.1208 (4)	0.3818 (5)	0.4123 (3)	0.0394 (14)	
H25	0.0829	0.4073	0.4431	0.047*	

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters (A^2)

C26	0.1969 (4)	0.4401 (4)	0.3935 (3)	0.0318 (12)	
H26	0.2108	0.5044	0.4119	0.038*	
C27	0.4222 (4)	0.4080 (4)	0.2802 (3)	0.0278 (11)	
H27A	0.3797	0.3680	0.2480	0.033*	
H27B	0.4632	0.4517	0.2567	0.033*	
C28	0.4891 (4)	0.3357 (4)	0.3247 (2)	0.0270 (11)	
H28A	0.5309	0.3752	0.3575	0.032*	
H28B	0.4485	0.2901	0.3471	0.032*	
C31	0.1094 (3)	0.5131 (4)	0.1110 (2)	0.0211 (10)	
C32	0.1117 (4)	0.5836 (4)	0.0602 (2)	0.0277 (11)	
H32	0.0979	0.6523	0.0668	0.033*	
C33	0.1343 (4)	0.5510 (4)	0.0005 (3)	0.0329 (12)	
H33	0.1368	0.5982	-0.0331	0.040*	
C34	0.1534 (4)	0.4484 (4)	-0.0101 (3)	0.0377 (14)	
H34	0.1681	0.4267	-0.0507	0.045*	
C35	0.1503 (4)	0.3783 (4)	0.0401 (3)	0.0373 (13)	
H35	0.1629	0.3094	0.0330	0.045*	
C36	0.1286 (4)	0.4100 (4)	0.1007 (3)	0.0290 (11)	
H36	0.1268	0.3627	0.1344	0.035*	
C37	0.0354 (3)	0.4546 (4)	0.2285 (2)	0.0243 (10)	
H37A	0.0844	0.4001	0.2321	0.029*	
H37B	0.0251	0.4746	0.2724	0.029*	
C41A	0.4293 (6)	0.5788 (5)	0.1447 (4)	0.025 (2)	0.508 (4)
C42A	0.3748 (4)	0.4987 (6)	0.1131 (4)	0.0391 (19)	0.508 (4)
H42A	0.3068	0.5057	0.1007	0.047*	0.508 (4)
C43A	0.4222 (5)	0.4079 (5)	0.1002 (4)	0.052 (3)	0.508 (4)
H43A	0.3857	0.3543	0.0791	0.062*	0.508 (4)
C44A	0.5239 (5)	0.3973 (5)	0.1188 (4)	0.044 (2)	0.508 (4)
H44A	0.5556	0.3366	0.1102	0.053*	0.508 (4)
C45A	0.5784 (4)	0.4775 (7)	0.1504 (4)	0.035 (3)	0.508 (4)
H45A	0.6465	0.4704	0.1628	0.042*	0.508 (4)
C46A	0.5311 (6)	0.5682 (6)	0.1633 (4)	0.0285 (12)	0.508 (4)
H46A	0.5675	0.6218	0.1844	0.034*	0.508 (4)
C41B	0.4365 (7)	0.6062 (6)	0.1305 (4)	0.025 (2)	0.492 (4)
C42B	0.3977 (5)	0.5663 (6)	0.0698 (4)	0.0391 (19)	0.492 (4)
H42B	0.3347	0.5859	0.0502	0.047*	0.492 (4)
C43B	0.4529 (6)	0.4970 (7)	0.0383 (3)	0.052 (3)	0.492 (4)
H43B	0.4270	0.4703	-0.0023	0.062*	0.492 (4)
C44B	0.5470 (5)	0.4676 (6)	0.0676 (4)	0.044 (2)	0.492 (4)
H44B	0.5840	0.4213	0.0465	0.053*	0.492 (4)
C45B	0.5858 (5)	0.5075 (7)	0.1283 (4)	0.035 (3)	0.492 (4)
H45B	0.6487	0.4879	0.1479	0.042*	0.492 (4)
C46B	0.5305 (7)	0.5768 (7)	0.1598 (3)	0.0285 (12)	0.492 (4)
H46B	0.5565	0.6036	0.2004	0.034*	0.492 (4)
C47	0.4461 (3)	0.7731 (4)	0.2149 (2)	0.0264 (11)	
H47A	0.4094	0.8192	0.2398	0.032*	
H47B	0.4882	0.7307	0.2458	0.032*	

Atomic displacement parameters $(Å^2)$

	U^{11}	U^{22}	U^{33}	U^{12}	U^{13}	U^{23}
Ag1	0.01757 (16)	0.02028 (19)	0.0306 (2)	-0.00137 (12)	0.00575 (13)	-0.00095 (13)
Sb1	0.0370 (2)	0.0407 (2)	0.0296 (2)	-0.00904 (16)	0.00059 (15)	0.00587 (15)
S1	0.0170 (5)	0.0194 (6)	0.0280 (6)	0.0012 (4)	0.0021 (4)	-0.0011 (4)
S2	0.0197 (6)	0.0202 (6)	0.0369 (7)	0.0017 (4)	0.0081 (5)	0.0011 (5)
S3	0.0186 (5)	0.0191 (6)	0.0307 (6)	-0.0026 (4)	0.0046 (5)	-0.0005 (4)
S4	0.0158 (5)	0.0276 (7)	0.0305 (6)	-0.0043 (4)	0.0028 (5)	0.0039 (5)
F1	0.079 (3)	0.044 (2)	0.072 (3)	0.024 (2)	-0.020 (2)	-0.0084 (19)
F2	0.069 (3)	0.106 (4)	0.067 (3)	-0.053 (3)	-0.006 (2)	0.015 (3)
F3	0.081 (3)	0.109 (4)	0.084 (3)	0.059 (3)	0.005 (3)	-0.019 (3)
F4	0.044 (2)	0.057 (2)	0.052 (2)	-0.0191 (18)	-0.0046 (17)	0.0042 (17)
F5	0.078 (3)	0.118 (4)	0.037 (2)	-0.032 (3)	-0.003 (2)	0.025 (2)
F6	0.056 (2)	0.050 (2)	0.038 (2)	-0.0002 (17)	-0.0038 (17)	0.0128 (15)
C11	0.024 (2)	0.018 (3)	0.023 (2)	0.0038 (18)	0.0019 (19)	-0.0032 (18)
C12	0.032 (3)	0.026 (3)	0.029 (3)	0.003 (2)	0.006 (2)	0.003 (2)
C13	0.039 (3)	0.038 (3)	0.037 (3)	0.007 (2)	0.017 (3)	0.003 (2)
C14	0.072 (5)	0.032 (3)	0.032 (3)	0.010 (3)	0.016 (3)	-0.001 (2)
C15	0.059 (4)	0.032 (3)	0.023 (3)	0.007 (3)	-0.009 (3)	-0.004 (2)
C16	0.039 (3)	0.024 (3)	0.033 (3)	0.001 (2)	-0.006 (2)	-0.004 (2)
C17	0.026 (3)	0.024 (3)	0.025 (3)	0.0081 (19)	0.003 (2)	-0.0015 (19)
C18	0.017 (2)	0.022 (3)	0.029 (3)	0.0027 (18)	0.0012 (19)	-0.0025 (19)
C21	0.021 (2)	0.021 (3)	0.031 (3)	0.0000 (18)	0.004 (2)	0.0051 (19)
C22	0.023 (2)	0.027 (3)	0.036 (3)	0.003 (2)	0.004 (2)	-0.001 (2)
C23	0.029 (3)	0.020 (3)	0.043 (3)	-0.004 (2)	-0.003 (2)	0.003 (2)
C24	0.031 (3)	0.025 (3)	0.046 (3)	-0.008 (2)	0.006 (2)	0.007 (2)
C25	0.042 (3)	0.044 (4)	0.036 (3)	-0.005 (3)	0.019 (3)	0.000 (3)
C26	0.039 (3)	0.020 (3)	0.039 (3)	-0.001 (2)	0.013 (2)	-0.001 (2)
C27	0.025 (3)	0.028 (3)	0.032 (3)	0.002 (2)	0.012 (2)	0.002 (2)
C28	0.021 (2)	0.028 (3)	0.032 (3)	0.0011 (19)	0.006 (2)	0.000 (2)
C31	0.014 (2)	0.020 (3)	0.028 (3)	-0.0007 (17)	0.0016 (18)	0.0035 (18)
C32	0.023 (2)	0.028 (3)	0.031 (3)	-0.0026 (19)	-0.001 (2)	0.008 (2)
C33	0.034 (3)	0.035 (3)	0.029 (3)	-0.012 (2)	0.000 (2)	0.009 (2)
C34	0.039 (3)	0.042 (4)	0.033 (3)	-0.019 (3)	0.009 (3)	-0.006 (2)
C35	0.045 (3)	0.025 (3)	0.042 (3)	0.002 (2)	0.009 (3)	-0.003 (2)
C36	0.031 (3)	0.020 (3)	0.037 (3)	0.0004 (19)	0.008 (2)	0.004 (2)
C37	0.022 (2)	0.028 (3)	0.022 (3)	-0.0086 (19)	0.0019 (19)	0.0016 (19)
C41A	0.018 (3)	0.031 (6)	0.027 (5)	-0.007 (3)	0.009 (3)	0.000 (4)
C42A	0.025 (4)	0.043 (5)	0.048 (5)	0.008 (3)	-0.003 (4)	-0.009 (3)
C43A	0.041 (5)	0.060 (7)	0.051 (6)	0.010 (4)	-0.010 (4)	-0.031 (4)
C44A	0.036 (5)	0.045 (6)	0.053 (6)	0.008 (4)	0.012 (4)	-0.012 (4)
C45A	0.023 (3)	0.050 (7)	0.033 (6)	-0.001 (4)	0.008 (4)	-0.005 (5)
C46A	0.022 (3)	0.030 (3)	0.032 (3)	-0.001 (2)	0.000 (2)	0.002 (2)
C41B	0.018 (3)	0.031 (6)	0.027 (5)	-0.007 (3)	0.009 (3)	0.000 (4)
C42B	0.025 (4)	0.043 (5)	0.048 (5)	0.008 (3)	-0.003 (4)	-0.009 (3)
C43B	0.041 (5)	0.060 (7)	0.051 (6)	0.010 (4)	-0.010 (4)	-0.031 (4)

C44B C45B C46B C47	0.036 (5) 0.023 (3) 0.022 (3) 0.019 (2)	0.045 (6) 0.050 (7) 0.030 (3) 0.026 (3)	0.053 (6) 0.033 (6) 0.032 (3) 0.033 (3)	0.008 (4) -0.001 (4) -0.001 (2) -0.0031 (19)	0.012 (4) 0.008 (4) 0.000 (2) 0.002 (2)	-0.012 (4) -0.005 (5) 0.002 (2) -0.004 (2)
Geometric para	meters (Å, °)					
Ag1-82		2 5293 (12)	C26—	-H26		0.93
Ag1—S3		2.5621 (12)	C27-	-C28		1 526 (7)
Ag1—S4		2.5639 (12)	C27—	-H27a		0.97
Ag1—S1		2.6170 (12)	C27—	-H27b		0.97
Sb1—F3		1.816 (4)	C28—	-C47 ⁱⁱ		1.517 (6)
Sb1—F5		1 864 (4)	C28	-H28a		0.97
Sb1—F6		1.866 (3)	C28	-H28b		0.97
Sb1—F4		1.866 (3)	C31–	-C36		1.392 (7)
Sb1—F2		1.886 (4)	C31–	-C32		1.395 (6)
Sb1—F1		1.929 (4)	C32—	-C33		1.374 (7)
S1—C11		1.799 (5)	C32—	-H32		0.93
S1—C17		1.814 (5)	C33—	-C34		1.387 (8)
S2—C21		1.786 (5)	C33—	-H33		0.93
S2—C27		1.802 (5)	C34—	-C35		1.385 (8)
S3—C31		1.781 (5)	C34—	-H34		0.93
S3—C37		1.820 (5)	C35—	-C36		1.384 (7)
S4—C41b		1.741 (6)	C35—	-H35		0.93
S4—C47		1.811 (5)	C36—	-H36		0.93
S4—C41a		1.831 (6)	C37—	-C18 ⁱⁱⁱ		1.530 (6)
C11—C12		1.378 (7)	C37—	-H37a		0.97
C11—C16		1.385 (7)	C37—	-H37b		0.97
C12—C13		1.374 (7)	C41a-	—C42a		1.39
С12—Н12		0.93	C41a-	—C46a		1.39
C13—C14		1.371 (8)	C42a-	—C43a		1.39
С13—Н13		0.93	C42a-	—H42a		0.93
C14—C15		1.379 (9)	C43a-	C44a		1.39
C14—H14		0.93	C43a-	—Н43а		0.93
C15—C16		1.384 (7)	C44a-	—C45a		1.39
C15—H15		0.93	C44a-	—H44a		0.93
C16—H16		0.93	C45a-	—C46a		1.39
C17—C18		1.523 (6)	C45a-	—H45a		0.93
С17—Н17а		0.97	C46a-	—Н46а		0.93
C17—H17b		0.97	C41b-	—C42b		1.39
C18—C37 ⁱ		1.530 (6)	C41b-	C46b		1.39
C18—H18a		0.97	C42b-	—C43b		1.39
C18—H18b		0.97	C42b-	—H42b		0.93
C21—C22		1.384 (7)	C43b-	C44b		1.39
C21—C26		1.390 (7)	C43b-	—H43b		0.93
C22—C23		1.396 (7)	C44b-	—C45b		1.39
С22—Н22		0.93	C44b-	—H44b		0.93
C23—C24		1.377 (7)	C45b-	C46b		1.39

С23—Н23	0.93	C45b—H45b	0.93
C24—C25	1.378 (8)	C46b—H46b	0.93
C24—H24	0.93	C47—C28 ^{iv}	1.517 (6)
C25—C26	1.380(7)	C47—H47a	0.97
С25—Н25	0.93	C47—H47b	0.97
S2—Ag1—S3	118.58 (4)	C25—C26—H26	120.2
S2—Ag1—S4	114.28 (4)	C21—C26—H26	120.2
S3—Ag1—S4	109.98 (4)	C28—C27—S2	112.5 (4)
S2—Ag1—S1	106.61 (4)	C28—C27—H27A	109.1
S3—Ag1—S1	103.08 (4)	S2—C27—H27A	109.1
S4—Ag1—S1	102.26 (4)	С28—С27—Н27В	109.1
F3—SB1—F5	92.2 (2)	S2—C27—H27B	109.1
F3—SB1—F6	90.18 (19)	H27A—C27—H27B	107.8
F5—SB1—F6	177.6 (2)	C47 ⁱⁱ —C28—C27	110.6 (4)
F3—SB1—F4	91.2 (2)	C47 ⁱⁱ —C28—H28A	109.5
F5—SB1—F4	89.82 (17)	C27—C28—H28A	109.5
F6—SB1—F4	90.21 (15)	C47 ⁱⁱ —C28—H28B	109.5
F3—SB1—F2	92.9 (2)	C27—C28—H28B	109.5
F5—SB1—F2	91.56 (18)	H28A—C28—H28B	108.1
F6—SB1—F2	88.24 (17)	C36—C31—C32	120.0 (5)
F4—SB1—F2	175.6 (2)	C36—C31—S3	123.9 (4)
F3—SB1—F1	178.1 (2)	C32—C31—S3	116.1 (4)
F5—SB1—F1	89.3 (2)	C33—C32—C31	119.8 (5)
F6—SB1—F1	88.32 (16)	С33—С32—Н32	120.1
F4—SB1—F1	87.73 (18)	С31—С32—Н32	120.1
F2—SB1—F1	88.2 (2)	C32—C33—C34	120.6 (5)
C11—S1—C17	103.9 (2)	С32—С33—Н33	119.7
C11—S1—AG1	105.44 (15)	С34—С33—Н33	119.7
C17—S1—AG1	104.63 (16)	C35—C34—C33	119.7 (5)
C21—S2—C27	104.6 (2)	C35—C34—H34	120.2
C21—S2—AG1	105.26 (16)	C33—C34—H34	120.2
C27—S2—AG1	108.28 (17)	C34—C35—C36	120.5 (5)
C31—S3—C37	104.4 (2)	С34—С35—Н35	119.7
C31—S3—AG1	103.08 (15)	С36—С35—Н35	119.7
C37—S3—AG1	109.11 (16)	C35—C36—C31	119.5 (5)
C41B—S4—C47	102.9 (3)	С35—С36—Н36	120.3
C47—S4—C41A	106.2 (3)	С31—С36—Н36	120.3
C41B—S4—AG1	115.2 (3)	C18 ⁱⁱⁱ —C37—S3	111.2 (3)
C47—S4—AG1	103.42 (16)	C18 ⁱⁱⁱ —C37—H37A	109.4
C41A—S4—AG1	100.2 (3)	S3—C37—H37A	109.4
C12—C11—C16	120.3 (5)	С18 ^{ііі} —С37—Н37В	109.4
C12—C11—S1	123.2 (4)	S3—C37—H37B	109.4
C16—C11—S1	116.5 (4)	Н37А—С37—Н37В	108
C13—C12—C11	119.9 (5)	C42A—C41A—C46A	120
C13—C12—H12	120.1	C42A—C41A—S4	116.6 (5)
C11—C12—H12	120.1	C46A—C41A—S4	123.3 (5)
C14—C13—C12	120.5 (6)	C41A—C42A—C43A	120

C14—C13—H13	119.8	C41A—C42A—H42A	120
C12—C13—H13	119.8	C43A—C42A—H42A	120
C13—C14—C15	119.8 (6)	C42A—C43A—C44A	120
C13—C14—H14	120.1	C42A—C43A—H43A	120
C15-C14-H14	120.1	C44A—C43A—H43A	120
C14—C15—C16	120.3 (5)	C45A—C44A—C43A	120
C14—C15—H15	119.8	C45A—C44A—H44A	120
C16-C15-H15	119.8	C43A—C44A—H44A	120
C15-C16-C11	119.2 (5)	C46A—C45A—C44A	120
C15-C16-H16	120.4	C46A—C45A—H45A	120
C11-C16-H16	120.4	C44A—C45A—H45A	120
C18—C17—S1	112.2 (3)	C45A—C46A—C41A	120
С18—С17—Н17А	109.2	C45A—C46A—H46A	120
S1—C17—H17A	109.2	C41A—C46A—H46A	120
С18—С17—Н17В	109.2	C42B—C41B—C46B	120
S1—C17—H17B	109.2	C42B—C41B—S4	114.9 (5)
H17A—C17—H17B	107.9	C46B—C41B—S4	125.1 (5)
$C17 - C18 - C37^{i}$	110.2 (4)	C43B—C42B—C41B	120
C17—C18—H18A	109.6	C43B—C42B—H42B	120
C_{27}^{i} C_{18} H_{18A}	109.6	$C_{41B} - C_{42B} - H_{42B}$	120
$C_{17} = C_{18} = H_{18}$	109.6	C42B C42B 1142B	120
	109.0		120
C37 ⁱ —C18—H18B	109.6	C42B—C43B—H43B	120
H18A—C18—H18B	108.1	C44B—C43B—H43B	120
C22—C21—C26	120.5 (5)	C43B—C44B—C45B	120
C22—C21—S2	124.4 (4)	C43B—C44B—H44B	120
C26—C21—S2	115.1 (4)	C45B—C44B—H44B	120
C21—C22—C23	118.9 (5)	C46B—C45B—C44B	120
C21—C22—H22	120.6	C46B—C45B—H45B	120
C23—C22—H22	120.6	C44B—C45B—H45B	120
C24—C23—C22	120.6 (5)	C45B—C46B—C41B	120
C24—C23—H23	119.7	C45B—C46B—H46B	120
C22—C23—H23	119.7	C41B—C46B—H46B	120
C25—C24—C23	120.0 (5)	C28 ^{iv} —C47—S4	112.7 (3)
C25—C24—H24	120	C28 ^{iv} —C47—H47A	109
C23—C24—H24	120	S4—C47—H47A	109
C24—C25—C26	120.4 (5)	C28 ^{iv} —C47—H47B	109
С24—С25—Н25	119.8	S4—C47—H47B	109
С26—С25—Н25	119.8	H47A—C47—H47B	107.8
C25—C26—C21	119.7 (5)		
S2—AG1—S1—C11	-41 29 (16)	C24 - C25 - C26 - C21	07(9)
S3—AG1—S1—C11	84 28 (16)	C^{22} C^{21} C^{26} C^{25}	-1.3(8)
S4—AG1—S1—C11	-161.55 (16)	82-C21-C26-C25	177 8 (4)
S2—AG1—S1—C17	-150 52 (17)	$C_{21} = S_{22} = C_{27} = C_{28}$	-739(4)
S3—AG1—S1—C17	-24 95 (18)	AG1—S2—C27—C28	174 3 (3)
S4—AG1—S1—C17	89 22 (17)	$S_{2}^{-} C_{27}^{-} C_{28}^{-} C_{47}^{ii}$	-1784(3)
S3 AG1 S2 C21	-20.62(18)	$C_{27} = C_{27} = C_{20} = C_{47}$	-220(5)
SJ = A G I = S2 = C2 I	20.02(10)	$C_{3} = C_{3} = C_{3$	-22.9(3)
34—AUI—32—U2I	-132.00 (17)	AUI-33-U31-U30	91.1 (4)

\$1AG1\$2C21	94 94 (18)	C_{37} S_{3} C_{31} C_{32}	157 5 (4)
$S_{1} = AG_{1} = S_{2} = C_{2}T$	90 76 (18)	AG1 = S3 = C31 = C32	-885(4)
S4 AG1 S2 C27	-41.50(10)	$C_{26}^{36} = C_{21}^{31} = C_{22}^{32} = C_{23}^{33}$	-1.0(7)
$S_{1} = AG_{1} = S_{2} = C_{2}^{7}$	-152.69(19)	$c_{30} - c_{31} - c_{32} - c_{33}$	1.0(7)
S1 = AO1 = S2 = C21	-133.08(18)	33-031-032-033	1/0.0 (4)
$S_2 = AG_1 = S_2 = C_2 I$	-94.01(10)	$C_{31} = C_{32} = C_{33} = C_{34}$	1.0(8)
S4—AG1—S3—C31	59.51 (10)	$C_{32} = C_{33} = C_{34} = C_{35}$	-0.5 (8)
SI—AGI—S3—C31	147.95 (16)	C33—C34—C35—C36	-0.2 (9)
S2—AG1—S3—C37	15.91 (18)	C34—C35—C36—C31	0.2 (8)
S4—AG1—S3—C37	150.04 (18)	C32—C31—C36—C35	0.4 (7)
S1—AG1—S3—C37	-101.52 (18)	S3—C31—C36—C35	-179.2 (4)
S2—AG1—S4—C41B	42.0 (3)	C31—S3—C37—C18 ⁱⁱⁱ	-64.9 (4)
S3—AG1—S4—C41B	-94.2 (3)	AG1—S3—C37—C18 ⁱⁱⁱ	-174.5 (3)
S1—AG1—S4—C41B	156.8 (3)	C41B—S4—C41A—C42A	-109 (2)
S2—AG1—S4—C47	-69.39 (17)	C47—S4—C41A—C42A	171.7 (4)
S3—AG1—S4—C47	154.36 (17)	AG1-S4-C41A-C42A	64.4 (4)
S1—AG1—S4—C47	45.38 (17)	C41B—S4—C41A—C46A	75 (2)
S2—AG1—S4—C41A	40.1 (3)	C47—S4—C41A—C46A	-4.4 (5)
S3—AG1—S4—C41A	-96.2 (3)	AG1-S4-C41A-C46A	-111.7 (4)
S1—AG1—S4—C41A	154.9 (3)	C46A—C41A—C42A—C43A	0
C17—S1—C11—C12	27.0 (5)	S4—C41A—C42A—C43A	-176.3 (6)
AG1-S1-C11-C12	-82.7 (4)	C41A—C42A—C43A—C44A	0
C17—S1—C11—C16	-154.1 (4)	C42A—C43A—C44A—C45A	0
AG1—S1—C11—C16	96.2 (4)	C43A—C44A—C45A—C46A	0
C16—C11—C12—C13	0.6 (8)	C44A—C45A—C46A—C41A	0
S1-C11-C12-C13	179.5 (4)	C42A—C41A—C46A—C45A	0
C11—C12—C13—C14	-1.3 (8)	S4—C41A—C46A—C45A	176.0 (6)
C12—C13—C14—C15	1.0 (9)	C47—S4—C41B—C42B	-152.3(4)
C13—C14—C15—C16	0.0 (9)	C41A— $S4$ — $C41B$ — $C42B$	103 (2)
C14—C15—C16—C11	-0.8(8)	AG1—S4—C41B—C42B	95.9 (5)
C12-C11-C16-C15	0 4 (7)	C47—S4—C41B—C46B	27.7 (6)
S1-C11-C16-C15	-1785(4)	C41A— $S4$ — $C41B$ — $C46B$	-77(2)
$C_{11} = S_{1} = C_{17} = C_{18}$	64 8 (4)	AG1—S4—C41B—C46B	-840(5)
AG1 = S1 = C17 = C18	175 1 (3)	C46B-C41B-C42B-C43B	0
$S1-C17-C18-C37^{i}$	-178.1(3)	S4—C41B—C42B—C43B	-179.9 (6)
$C_{27} = S_{2} = C_{21} = C_{22}$	-137(5)	C41B—C42B—C43B—C44B	0
AG1 = S2 = C21 = C22	10.7(5) 100 3 (4)	C42B - C43B - C44B - C45B	0
$C_{27} = S_{2} = C_{21} = C_{26}$	167.2 (4)	$C_{43B} = C_{44B} = C_{45B} = C_{46B}$	0
$C_2 = C_2 $	-78.8(4)	C43B - C44B - C45B - C40B	0
A01 - 52 - C21 - C20	-70.0(4)	C44B - C45B - C40B - C41B	0
$C_{20} - C_{21} - C_{22} - C_{23}$	-178 A (A)	$C_{42}D - C_{41}D - C_{40}D - C_{43}D$	(7)
52 - 021 - 022 - 023	-1/0.4 (4)	54 - C41D - C40B - C45B	1/9.9(/)
C21—C22—C23—C24	0.5 (8)	C41B—S4—C47—C28 ¹	03.1 (5)
C22—C23—C24—C25	-1.1 (8)	C41A—S4—C47—C28 ^{1V}	80.4 (5)
C23—C24—C25—C26	0.5 (9)	AG1—S4—C47—C28 ^{iv}	-174.7 (3)
Symmetry codes: (i) $-x$, $y+1/2$, $-z+1/2$; (ii) $-x+1$, $y-1/2$, $-z+1/2$; (iii) $-x$, $y-1/2$, $-z+1/2$; (iv) $-x+1$, $y+1/2$, $-z+1/2$.			



Fig. 2





Fig. 3